

Swelling of self-adhesive resin cement increases long-term push-out bond strength of fiber post to dentin

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Abstract

Aim: To evaluate the long-term post push-out bond strength to dentin, water sorption, solubility and swelling of conventional and self-adhesive dual-cure resin cements. **Methods:** Forty-eight bovine roots were prepared for fiber post cementation with RelyX ARC and RelyX U100. According to resin cement and storage time (24 h and 6 months), 4 groups were assessed using the push-out test. Water sorption and solubility were performed according to ISO 4049:2009. The swelling coefficient was obtained using cement disks of each material immersed in distilled water until the swelling equilibrium was reached. The mass of dry and swelled polymer and solvent density were used to calculate the coefficient. Statistical data analysis was performed using Student's t-test for water sorption, solubility and swelling coefficient and the Kruskal-Wallis and Dunn multiple comparison tests for push-out analysis with a significance level of 0.05. **Results:** The immediate bond strength was not significantly different between RelyX ARC (3.09 MPa) and RelyX U100 (3.78 MPa) ($p>0.05$). RelyX U100 showed higher ($p<0.05$) bond strength after six months of storage (9.60 MPa) than RelyX ARC (6.65 MPa). The water sorption and solubility values were not significantly different ($p>0.05$) between groups. The swelling coefficient of the RelyX U100 group was significantly higher than that of the RelyX ARC group ($p<0.05$). **Conclusions:** RelyX U100 resin cement showed a higher swelling coefficient than RelyX ARC, and the longitudinal push-out bond strength increased after six months. Clinical significance: The clinical longevity of restorative treatment in root-filled teeth is dependent on the long-term properties and behavior of the cement used for post luting. Results of this study suggest that the self-adhesive resin cement may be a reliable alternative.

Keywords: resin cements; dentin-bonding agents; solubility; water storage.

Introduction

Fiber posts are widely used to restore endodontically treated teeth as an alternative to metal posts and cores. The similarity in the elastic modulus among the fiber post, resin cement and dentin is advantageous for the improved performance of restorative procedures¹. Moreover, the chemical nature of the posts allows them to be bonded to canal walls with adhesive systems in combination with resin cements.

The choice of a luting agent depends on the clinical situation and on the material's physical, biologic and handling properties. In general, the resin cements are composed of a dimethacrylate-based polymeric matrix, filler particles, pigments

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and chemical substances to start the polymerization reaction. Variation in the content of these components strongly influences the physicochemical properties of the material².

The use of conventional resin cements requires pretreatment of the root surface with an adhesive system³ to increase the bond strength⁴. The adhesion strategy of etch-and-rinse adhesive systems involves two or three steps with the successive application of an acid, followed by a primer and an adhesive resin. In self-etch adhesive systems, the etching and priming steps are combined, and in the most recent formulations, etching, priming, and bonding are combined into a single step⁵.

Recently introduced self-adhesive resin cements do not require the pretreatment of the tooth substrate. The adhesive properties of self-adhesive cements are attributed to acidic methacrylate monomers that simultaneously demineralize and infiltrate the tooth substrate, resulting in micromechanical retention⁶. Self-adhesive resin cements present reliable immediate bond strength to dentin^{1,7,8}. However, the longevity of bond strength is still a concern for cementation procedures.

Therefore, the purpose of this study was to evaluate the long-term push-out bond strength of post to dentin with conventional and self-adhesive dual-cure resin cements.

Material and methods

Specimen preparation

Forty-eight bovine teeth with similar lengths and dimensions were used in this study. Freshly extracted teeth were immediately immersed in distilled water and stored at 4 °C for no more than 6 months. To be included in this study, the following criteria had to be met: straight roots and root length of at least 15 mm. External debris were removed with a periodontal curette. The crown surfaces of each tooth were sectioned below the cementum-enamel junction, perpendicular to their long axis, using a low speed diamond disc with water coolant.

After endodontic access, the working length was established by the direct method subtracting 1 mm from the real root length, determined by introducing a n° 10 K-file (Maillefer-Dentsply, Ballaigues, Switzerland) until the file was visible through the apical foramen. The root canals were prepared with K-files using the step-back technique. The

coronal portion of each canal was shaped with size 2 Gates-Glidden drills. The root canals were irrigated with 3 mL distilled water prior to each instrument. After final irrigation, the root canals were dried with absorbent paper points.

Cementation of fiber posts

The post space of each specimen was enlarged with a n° 2 drill from the Exacto post system (Angelus, Londrina, PR, Brazil), 4 mm before reaching the working length depth. The fiber post was 20 mm long, 1.4 mm cervical diameter, and 0.9 mm apical diameter. To standardize the method, the same operator performed all of the procedures. Following post space preparations, the roots were randomly divided into 4 experimental groups of 12 teeth, according to material and storage time (n = 12).

The resin cements were applied according to the manufacturer's instructions and are shown in Table 1. The fiber posts were cleaned with 96% ethanol, and silane was applied with disposable microbrush tips⁹. In the RelyX ARC (3M ESPE) groups, the intracanal dentin was etched with 37% phosphoric acid for 15 s, rinsed with distilled water for 15 s, and then gently dried with absorbent paper points. The activator (3M ESPE) was applied to the canal with a paper point and gently air-dried followed by application of the primer (Scotch Bond Multi-Purpose Plus, 3M ESPE). The catalyst (3M ESPE) was applied on the root dentin and the post.

The cements were inserted only into the root canal¹⁰ with Accudose (Centrix Inc, Shelton, CT, USA) needle tubes and a Centrix syringe (Centrix Inc, Shelton, CT, USA)¹¹. The fiber post was inserted and excess cement was removed. Light activation was performed through the cervical portion of the root for 30 s at the buccal and lingual surfaces for a total of 60 s of light exposure, with a 5 mm distance between the source and the root. The resin cement and adhesive were light activated with XL2500 (3M ESPE), with an output intensity of 600 mW/cm². The power of the light curing unit was gauged with a radiometer (Model 100, Demetron Research Group, Danbury, CT, USA).

Push-out test

All the roots in all groups were stored in 37 °C distilled water for 7 days and then serially sectioned into 0.7 mm-thick slices in a precision cutting machine (Low Speed Saw,

Table 1: Chemical compositions of materials

Material		Composition
RelyX ARC	Paste A	BISGMA, TEGDMA, silane treated ceramic, silane treated silica, functionalized dimethacrylates polymer, triphenylantimony.
	Paste B	BISGMA, TEGDMA, silane treated silica, silane treated ceramic, functionalized dimethacrylates polymer, benzoyl peroxide.
RelyX U100	Base	Glass powder, methacrylated phosphoric acid esters, triethylene glycol dimethacrylates, silane treated silica, sodium persulfate.
	Catalyst	Glass powder, substituted dimethacrylate, silane treated silica, sodium p-toluenesulfonate, calcium hydroxide.
Scotch Bond		
Multi-Purpose Plus	Primer	HEMA, copolymer of acrylic and itaconic acids, water.
	Catalyst	BISGMA, HEMA, benzoyl peroxide, triphenylphosphine, triphenylantimony, hydroquinone.
	Activator	Ethyl alcohol, sodium benzenesulfonate.

Buehler, Lake Bluff, IL, USA) with constant water cooling. The slices of all roots from each group were stored in 37 °C distilled water for 24 hours or 6 months before the push-out tests. The cervical and apical diameters of the canal and the thickness of all of the slices were measured with a digital caliper. Each section was marked on its apical side and positioned on a base with a central hole in a universal testing machine (DL2000, EMIC, São José dos Pinhais, PR, Brazil). The push-out test was performed applying a compressive load to the apical side of each slice using a 0.7 mm-diameter cylindrical plunger attached to the upper portion of the testing machine. A crosshead speed of 0.5 mm/min was applied until bond failure occurred. To express the bond strength in MPa, the load upon failure was recorded in Newton (N) and divided by the bond area (mm²)¹².

Water Sorption and Solubility

Water sorption and solubility were determined based on the ISO 4049:2009 standard specification, except for specimen size. Cement disks (n=5) of each material were produced in a polytetrafluoroethylene matrix (6.0 mm diameter and 1-mm thick, in order to fit the light output guide of the QTH curing unit). For specimen preparation, the cement was directly dispensed into the mold until it was filled. An acetate strip was placed on top of the cement and covered with a glass slide. The specimens were light activated for 20 s, removed from the mold and the opposite surface received additional light activation for 20 s.

Specimens were placed in a desiccator containing silica gel at 37 °C. The disks were repeatedly weighed after 24-h intervals on an analytical scale until a constant mass (m1) was obtained (i.e., until the mass loss of each specimen was not more than 0.1 mg in any 24-h period). The diameter and thickness of each specimen were measured with a digital caliper to calculate the volume (V) of each disk (in mm³). Thereafter, the specimens were stored in sealed glass vials with 10 mL distilled water at 37 °C for 7 days. After seven days, the disks were weighed after being washed under running water and gently wiped with an absorbent paper to obtain the mass measure (m2) and then returned to the desiccator. Next, the specimens were weighed until a constant mass (m3) was obtained (as described above). Water sorption (WS) and solubility (SL) were calculated in micrograms per cubic millimeter¹³.

Swelling coefficient

Swelling coefficient measurements were performed gravimetrically. Cement samples (n=3) of each material were produced in a polytetrafluoroethylene matrix (2 x 2 x 12 mm). Next, the samples were immersed in distilled water at 37 °C until swelling equilibrium was reached. Then, the samples were removed, the excess solution deposited on the film surface was quickly removed with blotting paper and the samples were weighed.

The values of the swelling coefficients (α) of all materials were calculated using the following equation:

$$\alpha = ((M_{eq} - M_0) / M_0) \times 1/d_s$$

Where M_{eq} is the mass of the sample (polymer + solvent) after equilibrium, M_0 the mass of the polymer, and d_s is the density of the solvent¹⁴.

Statistical analysis

Statistical analysis was performed using SigmaStat (version 4, Ashburn, GA, USA). The normality of the results was tested using the Kolmogorov-Smirnov test. The used statistical tests were Student's t-test for water sorption, solubility and swelling coefficient and the Kruskal-Wallis and Dunn multiple comparison tests for push-out analysis, all at a significance level of 0.05.

Results

The results of the bond strength analysis are presented in Figure 1. The RelyX ARC group exhibited 3.09 (± 1.72) MPa at 24 h and 5.65 (± 5.77) MPa at 6 months ($p > 0.05$). The RelyX U100 group presented 3.78 (± 1.84) MPa and 9.60 (± 7.65) MPa at 24 h and 6 months ($p < 0.05$), respectively.

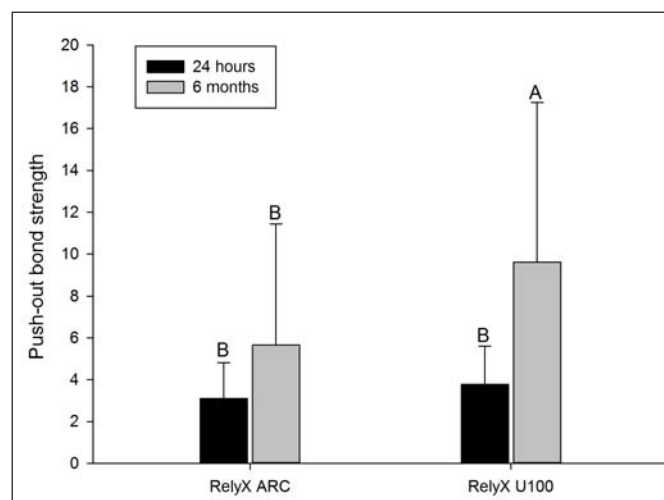


Fig. 1: Bond strength values as a function of evaluation period and cement type. Different letters represents statistically significant difference among groups ($p < 0.05$).

Water sorption and solubility showed no statistical differences ($p > 0.05$) between cements. The swelling coefficient of the RelyX U100 group (0.027 mLg) was significantly higher than that of the RelyX ARC group (0.011 mLg) ($p < 0.05$). The means and standard deviations are shown in Table 2.

Table 2: Mean and standard deviation ($\pm$ SD) of water sorption (WS), solubility (SL) and swelling coefficient (α) of the resin cement

Group	WS ($\mu\text{g}/\text{cm}^3$)	SL ($\mu\text{g}/\text{cm}^3$)	α (mLg)
RelyX ARC	19.27 (± 1.39)	2.19 (± 0.45)	0.011 (± 0.00006)
RelyX U100	19.94 (± 2.98)	0.86 (± 1.48)	0.027 (± 0.00172)
p	0.66	0.09	0.000

Discussion

The clinical longevity of restorative treatment in root-filled teeth relies on the properties of the used cement³. Water movement from the intra-radicular dentin through the hybrid layer is one of the reasons for cement/dentin interface degradation over time¹⁵. In this study, the tested resin cements showed similar water sorption, solubility and immediate push-out bond strength. Nevertheless, RelyX U100 demonstrated higher swelling coefficients and longitudinal push-out bond strength values than RelyX ARC.

Water sorption of polymers could lead to degradation¹⁵. Furthermore, the polymer could undergo hygroscopic expansion^{2,16} due to the chemistry of monomers and polymerization linkages¹⁷. Monomers like HEMA, Bis-GMA and TEGDMA are heteroatom structures composed of carbon and oxygen¹⁵ revealing the presence of hydrolytically susceptible ester groups¹⁸. Water sorption of resin composites depends on the degree of conversion of the polymer, the polar interaction, the particle size and morphology of the filler, and the surface area exposed to water¹⁷. In this study, all specimens presented water sorption after seven days of storage.

The swelling coefficient was calculated based on the mass of the polymer before and after immersion, when the polymer shows a constant swelling mass. In this study, the resin cements only presented a stable mass after 29-day immersion. RelyX U100 presented higher swelling coefficient than RelyX ARC. Self-adhesive resin cement contains acidic monomers (e.g., carboxylated or phosphate-derivatized methacrylates) in its composition, which have polar structures, leading to increased water sorption¹⁹.

Retention of fiber posts in roots depends on the bond strength between post material and a resin luting agent, bond strength between post space dentin and resin luting agent¹. Despite the difference in the mechanism of adhesion of both tested materials, immediate push-out bond strength presented no difference in this study, corroborating other studies^{12,20-24}. Although resin cements present reliable immediate results, the longevity of the bond strength should be evaluated. Adhesive interfaces are prone to degradation over time, leading to a decrease in bond strength. One could think that 6 months of water storage could decrease the push-out bond strength of resin cements. However, in this study, six months of storage significantly increased the bond strength values for the RelyX U100 group.

According to a systematic review there is a 3.81 MPa increase of resistance to dislodgement for bovine teeth when compared to human teeth²⁵. The increase in value is proportional to the used type of teeth. In the present study, bovine teeth were used in all groups.

Considering the water sorption value (19.94 $\mu\text{g}/\text{cm}^3$) and low solubility (0.86 $\mu\text{g}/\text{cm}^3$), RelyX U100 presented hygroscopic expansion leading to material swelling. The hygroscopic behavior of materials is strongly influenced by filler composition¹⁷. The self-adhesive resin cement used in this study contains fluoroaluminosilicate glass powder, which exhibits hygroscopic expansion²⁶. Glass-ionomer and resin-

modified glass-ionomer luting cements presented delayed hygroscopic expansion increasing fiber post retention²⁷. The hygroscopic expansion could explain the increased long-term bond strength values showed in this study. The RelyX ARC group exhibited lower push-out bond strength values after six months of storage, suggesting that a concurrent solubility (2.19 $\mu\text{g}/\text{cm}^3$) process occurred during the water sorption stage²⁸. The sorption and solubility features of resin cements have been studied²⁹, and the structural characteristics of polymers are essential to determine the extent to which polymers are affected by an aqueous environment¹⁷. Other parameters, such as the cross-linking density of the polymeric network²⁹, the amount of monomers³⁰ and polarity of functional groups may affect the cement behavior. The results presented by RelyX ARC are in agreement with the current literature³¹⁻³².

Despite the materials' degradation over time, the self-adhesive resin cement showed higher bond strength after six months, presenting a high swelling coefficient and low solubility. Considering that the leachability of dental polymers is a biological concern, polymers with low release of components are required.

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